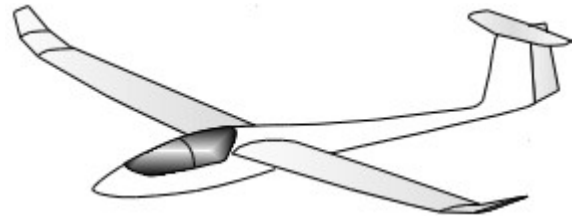


Why does an airfoil drag: the viscous problem



CFD « RANS »
Reynolds Averaged
Navier-stokes solvers

Navier-Stokes equations

Inviscid fluid

Time averaged
turbulence

Euler's equations

Reynolds equations

irrotational flow
 $\vec{V} = \nabla\phi$

Potential flow

3d Boundary Layer eq.

Viscosity models, uniform
pressure in BL thickness, Prandtl
mixing length hypothesis.

Time independent,
incompressible flow

Laplace's equation
 $\Delta\phi = 0$

2d BL equations

1d BL Integral
equations

2d BL differential
equations

mixed empirical + theoretical
turbulence and transition models

2d, 3d
xflr5

2d viscous results
interpolation

XFOIL
Subsonic Airfoil Development System

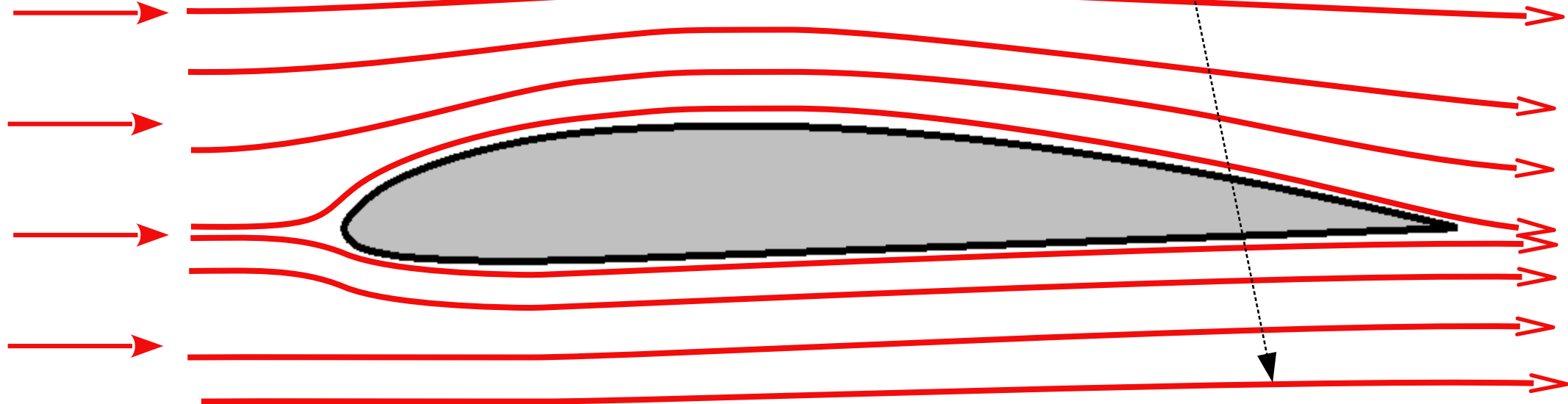
The inviscid flow around an airfoil

Favourable pressure gradient, the flow accelerates from zero at the leading edge's stagnation point.

Adverse pressure gradient, the flow decelerates



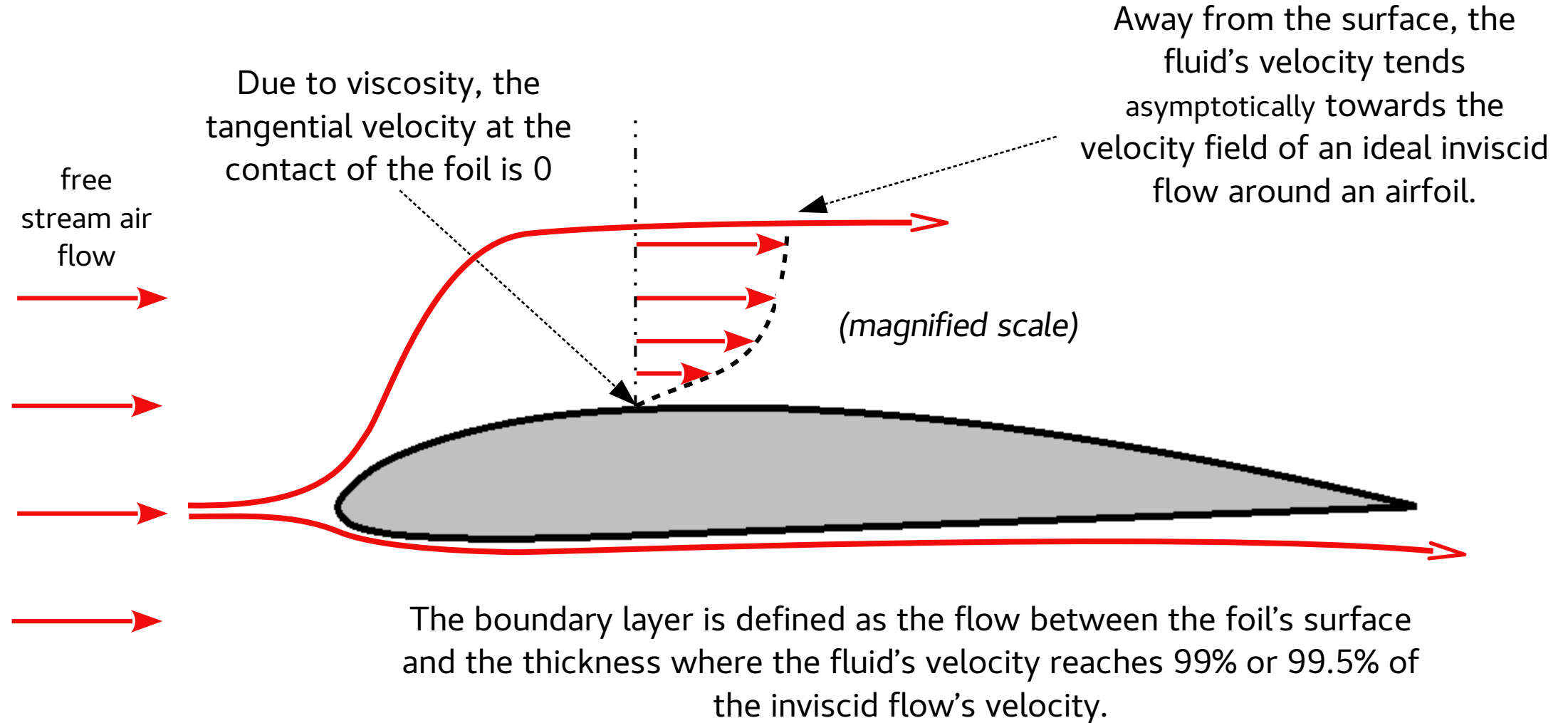
free
stream air
flow



Away from the surface, the flow tends asymptotically towards the freestream uniform flow

inviscid \leftrightarrow "laminar",

The boundary layer



The viscous flow around an airfoil at low Reynolds number

Favourable pressure gradient, the flow accelerates from zero at the leading edge's stagnation point.

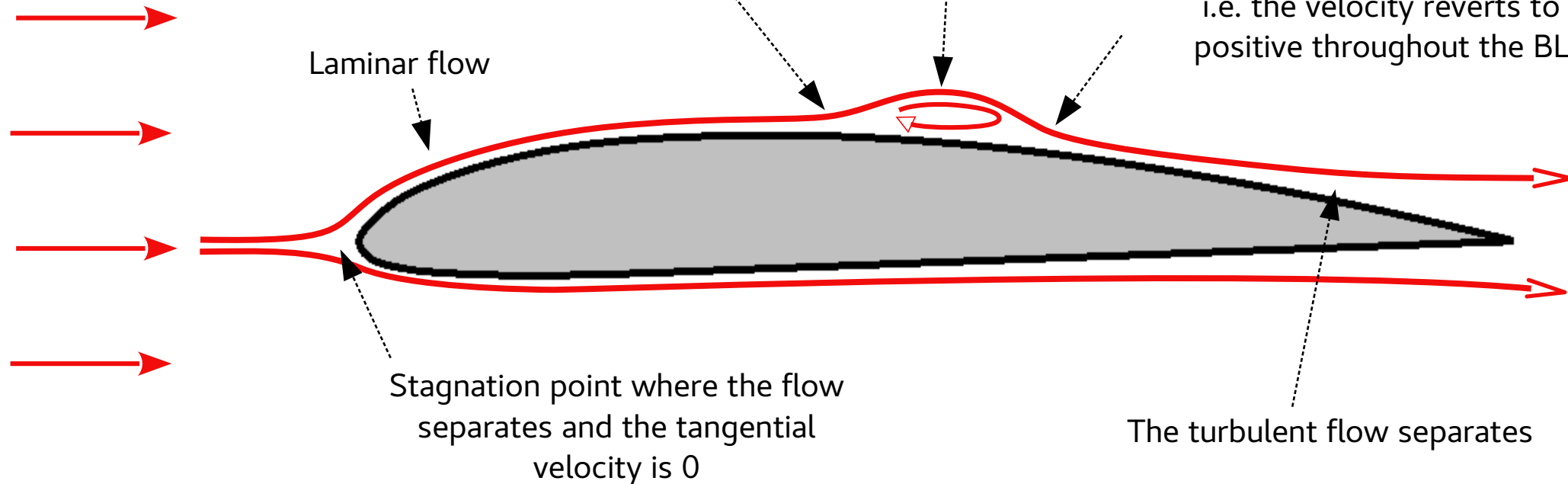
Adverse pressure gradient, the flow decelerates



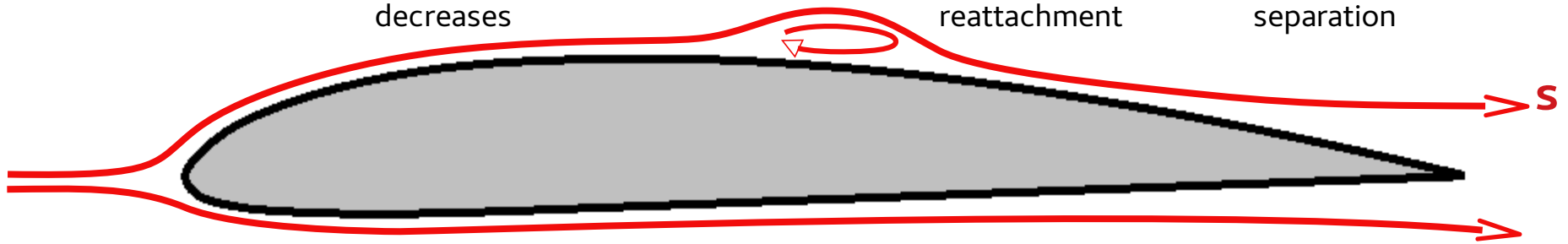
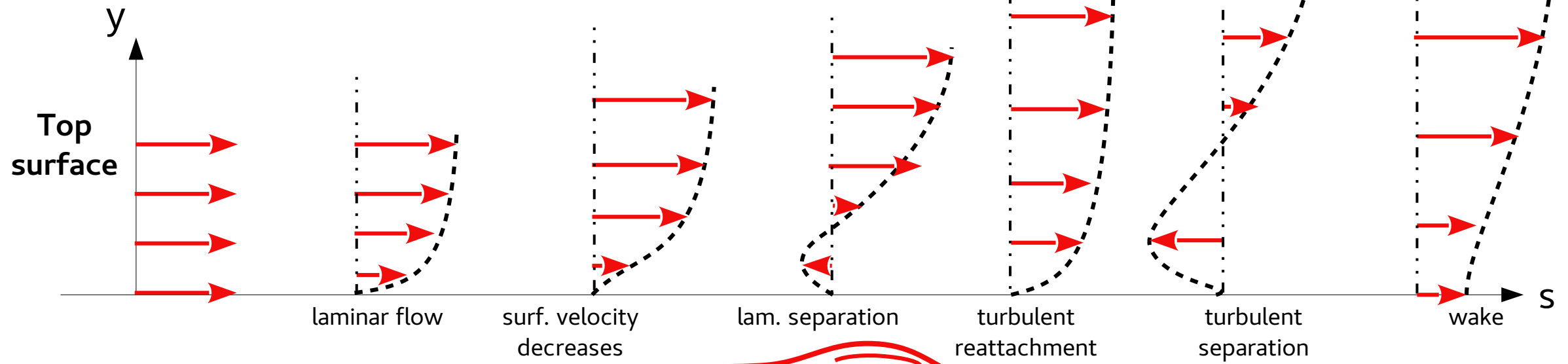
In adverse pressure gradients, the laminar flow separates. The velocity close to the surface goes negative.

A separation bubble forms. The flow goes progressively turbulent inside the bubble.

The turbulent flow reattaches, i.e. the velocity reverts to positive throughout the BL



The viscous flow around an airfoil



Things to note

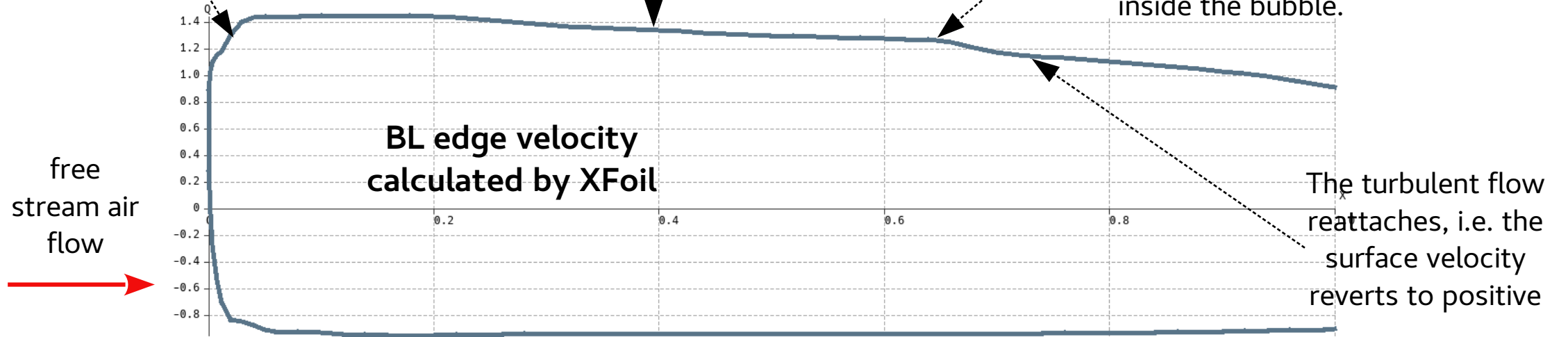
- The BL thickness increases progressively
- No surface slip on the airfoil surface

The viscous flow around an airfoil

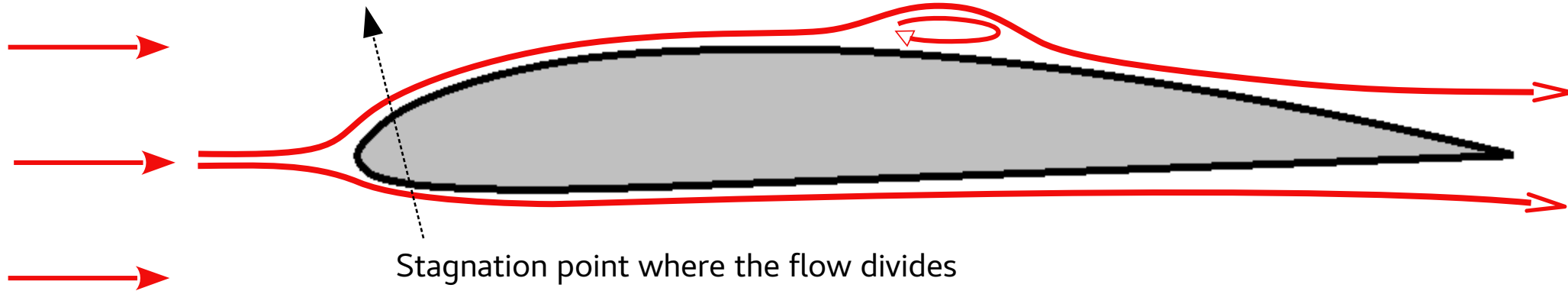
Favorable pressure gradient, the flow accelerates.

Adverse pressure gradient, the flow decelerates and separates.

A separation bubble forms. The flow goes progressively turbulent inside the bubble.



The turbulent flow reattaches, i.e. the surface velocity reverts to positive



Stagnation point where the flow divides and the tangential velocity is 0

The viscous flow around an airfoil

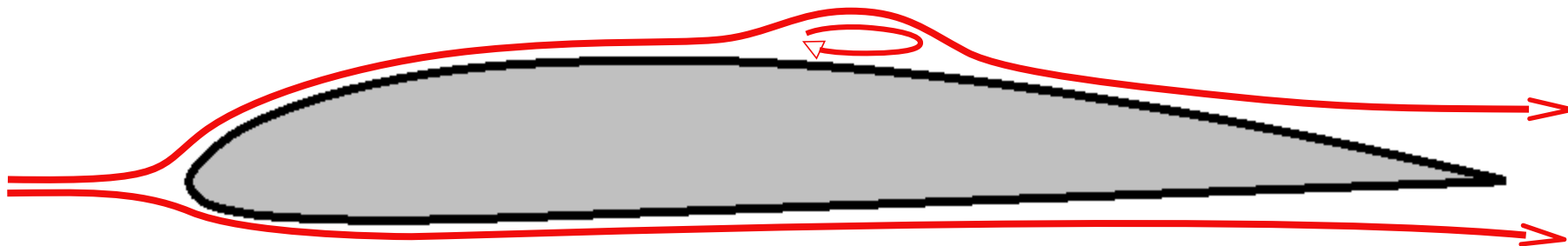
The transition problem

The transition from laminar to turbulent flow is a complex problem in 2d and even more so in 3d.

Things to note in 2d:

- Transition occurs when the amplification factor of spatial waves known as Tollmien–Schlichting waves reaches a critical value, i.e. the $NCrit$ factor
- Turbulent flow starts with small “sparks” which eventually extend downstream to full turbulence

free
stream air
flow



- “For low Reynolds number flows, the transition is separation induced”
(in.T. Cebeci, Modeling and computation of boundary-layer flows, chapter.5.2)
This is also what Xfoil predicts

The 2d problem

The 2d inviscid potential problem can be solved numerically for the velocity field by solving Laplace's equation



The velocity field is used as an input to solve the BL problem



The 2d problem

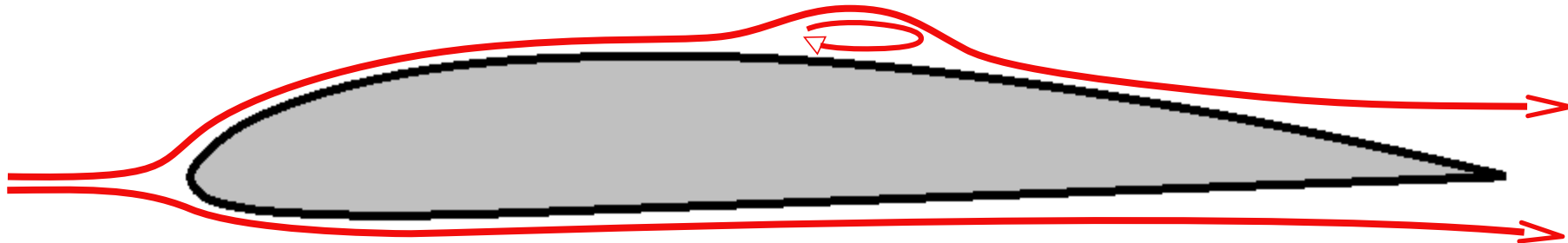
The 2d inviscid potential problem can be solved numerically for the velocity field



The velocity field is used as an input to solve the BL problem

In the 1940s, theoreticians have found that this method does not converge in adverse pressure gradients, e.g. on the upper surface of an airfoil.

This problem is known as the “Goldstein singularity”



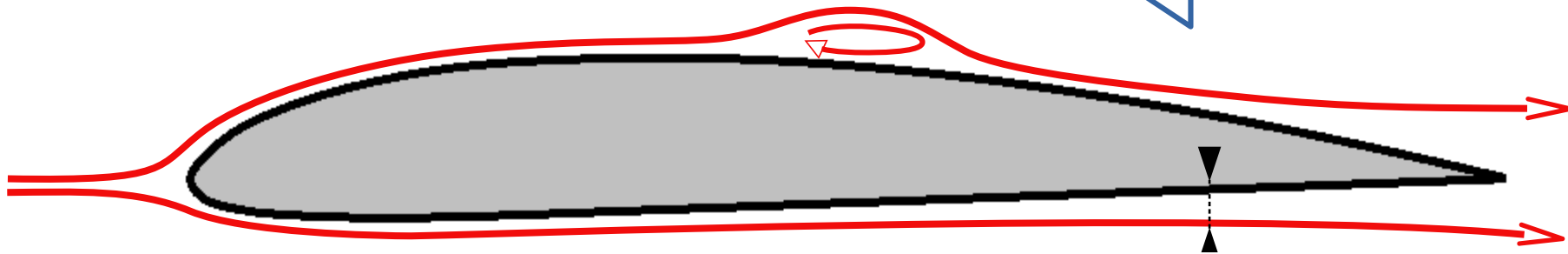
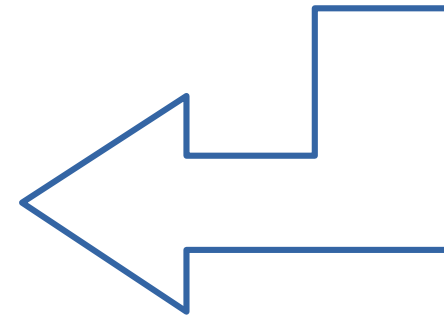
The 2d problem

The 2d inviscid potential problem can be solved numerically for the velocity field



The velocity field is used as an input to solve the BL problem

The reason is that the BL disturbs the inviscid flow: the foil behaves as if it had an additional thickness



The inviscid flow wants to dictate its law to the BL, but the BL does not agree, and vice versa.

This additional thickness is called the “displacement thickness δ^* ”
Note: not the same thing as the BL thickness

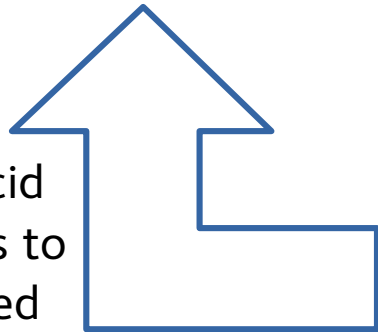
The 2d problem

The 2d inviscid potential problem can be solved numerically for the velocity field

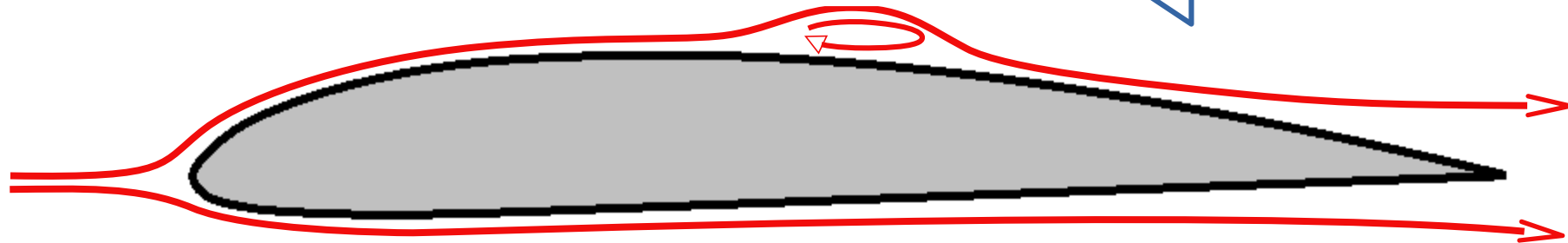
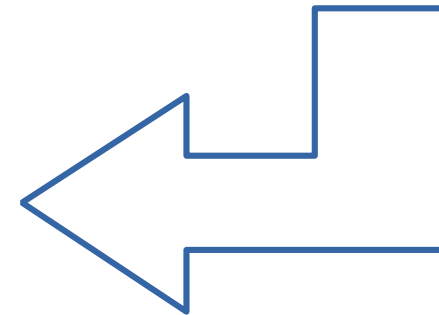


The velocity field is used as an input to solve the BL problem

The inviscid flow needs to be updated



The reason is that the BL disturbs the inviscid flow: the foil behaves as if it had an additional thickness



This iterative method is called the “Interactive Boundary Layer”, or IBL

The 2d problem

Many schemes have been proposed for the IBL problem

“Direct” :

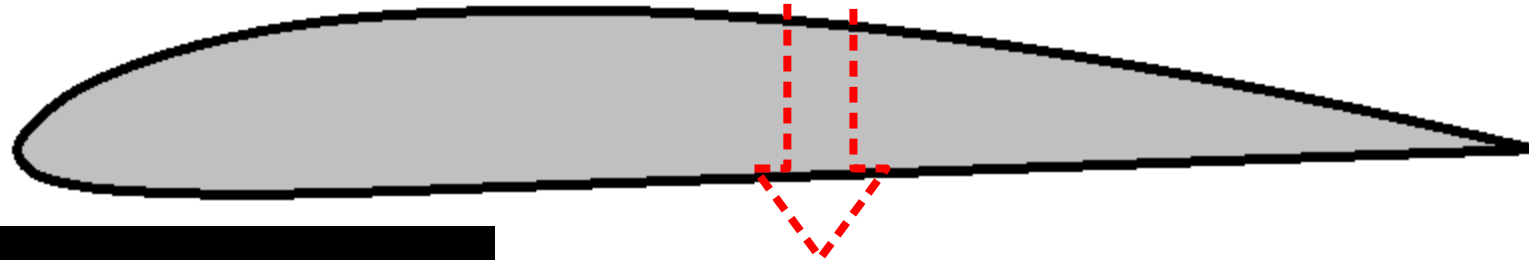
The inviscid velocity is used as an input for the BL solver

“Inverse”

The viscous velocity from the BL solution is used as an input for the potential flow solver

“Simultaneous” :

The inviscid and BL equations are solved concurrently at each iteration

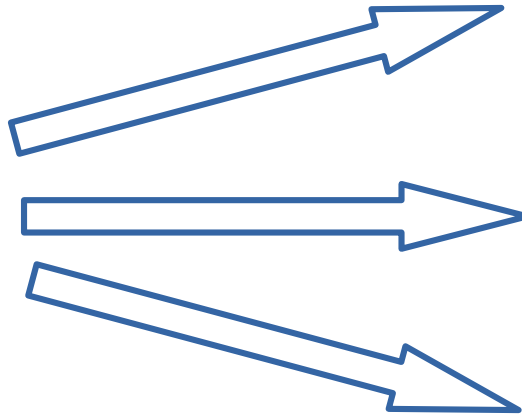


Developed by M. Drela and H. Youngren in the 1990s, XFOIL is still a (the?) state-of-the-art IBL solver some 30 years later

XFOIL
Subsonic Airfoil Development System

About XFOIL

Three main things which make XFOIL outstanding



A comprehensive set of 2d BL turbulence and transition models

A full simultaneous IBL solver

A robust and reliable software package



http://web.mit.edu/drela/Public/papers/xfoil_sv.pdf

About XFOIL

XFOIL's 1D Integral method

BL equations are integrated in the BL thickness

BL properties are therefore function only of the streamwise position "s"

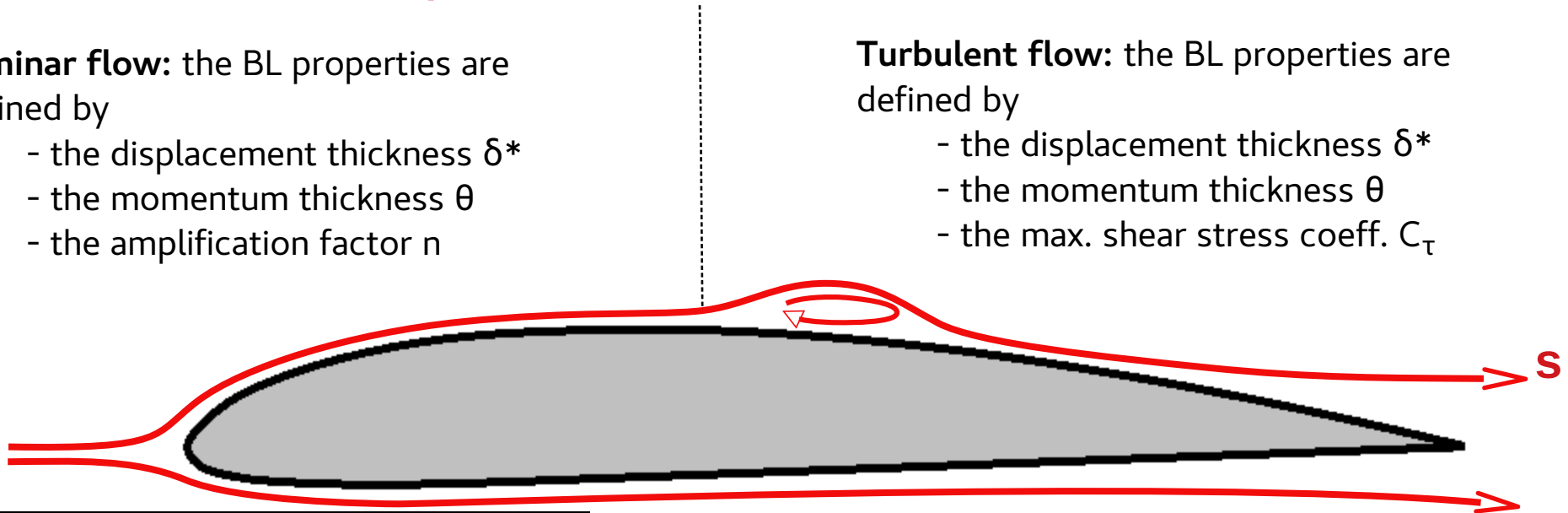
3 variables, one space dimension

Laminar flow: the BL properties are defined by

- the displacement thickness δ^*
- the momentum thickness θ
- the amplification factor n

Turbulent flow: the BL properties are defined by

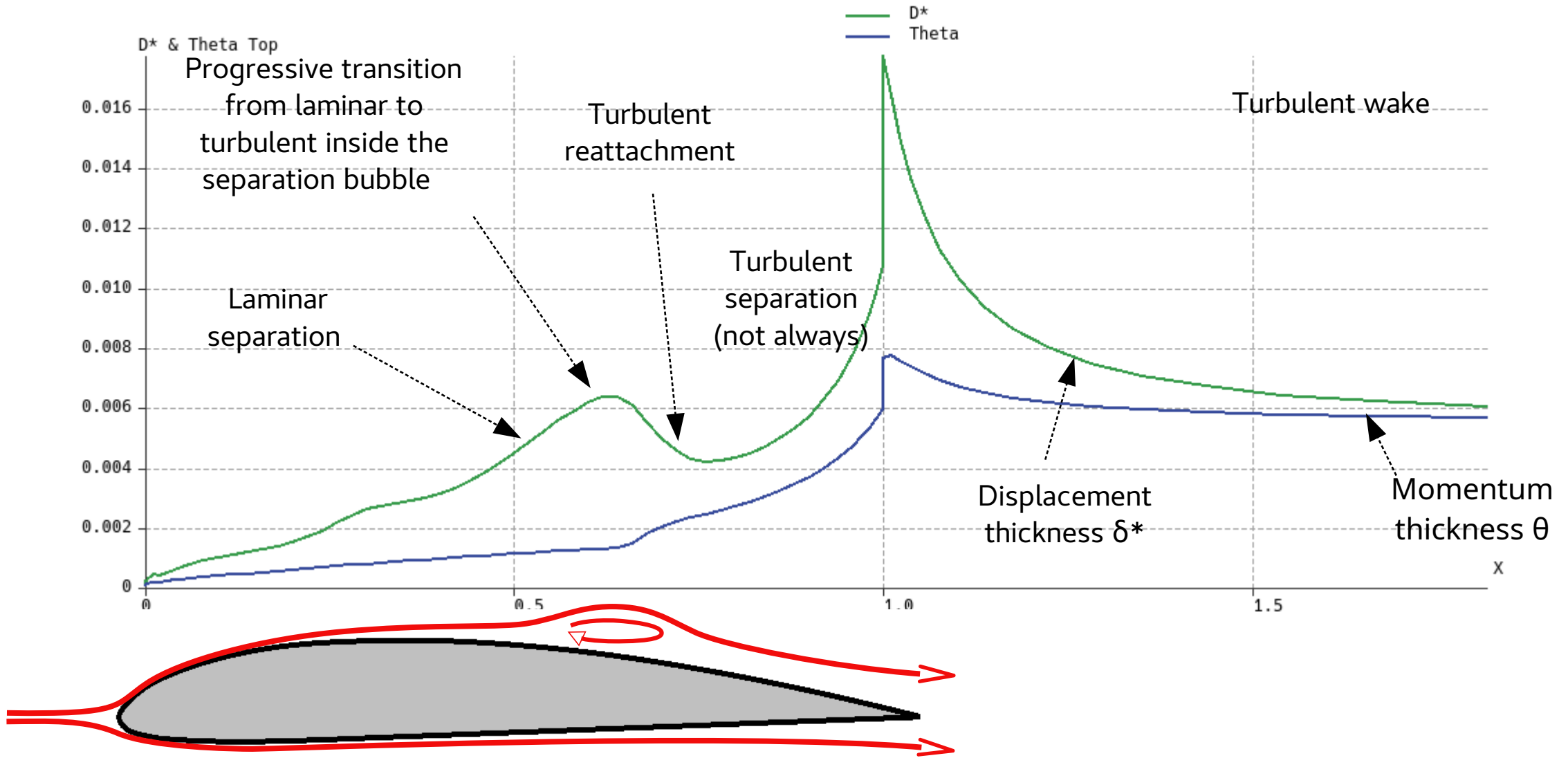
- the displacement thickness δ^*
- the momentum thickness θ
- the max. shear stress coeff. C_τ



http://web.mit.edu/drela/Public/papers/xfoil_sv.pdf

About XFOIL

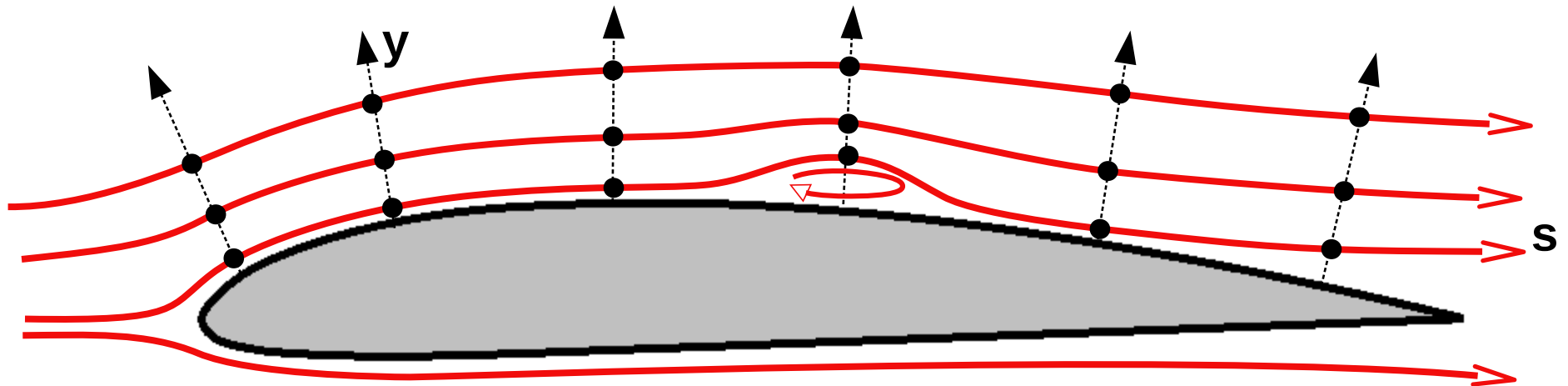
Standard behaviour of
a BL at low Re



Differential solvers

With the increase of computing power, it has become possible to solve the BL equations without prior integration in the thickness.

BL properties are defined at each position (s, y) .

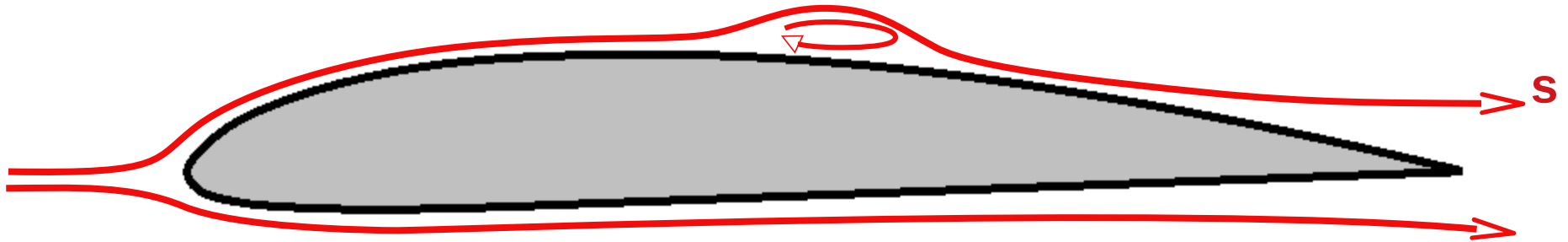


Although they require less empirical assumptions than integral methods, differential solvers still need a turbulence model which is the key building brick of the method.

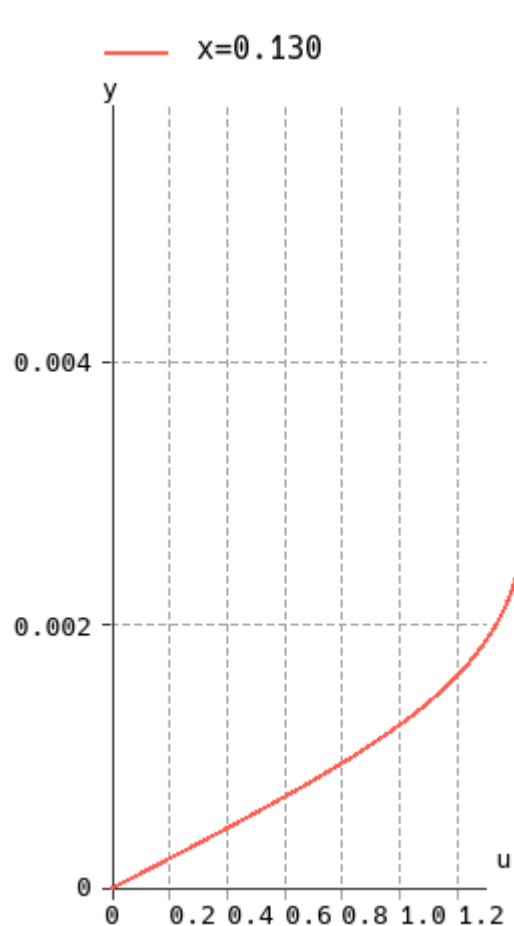
Differential solvers

The results which follow are from a differential solver currently in development.

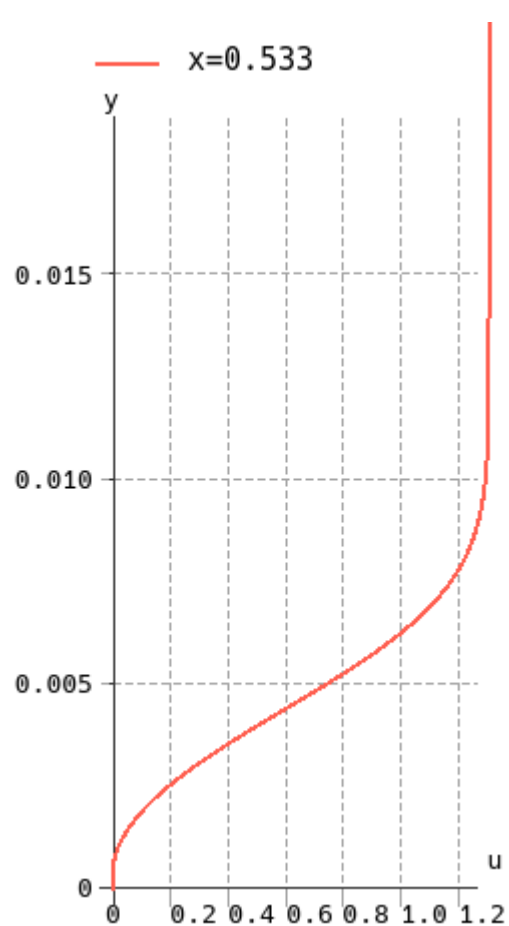
- The solver is based on the methods proposed by T. Cebeci in “Modeling and computation of boundary-layer flows”
- It uses the Cebeci-Smith turbulence model



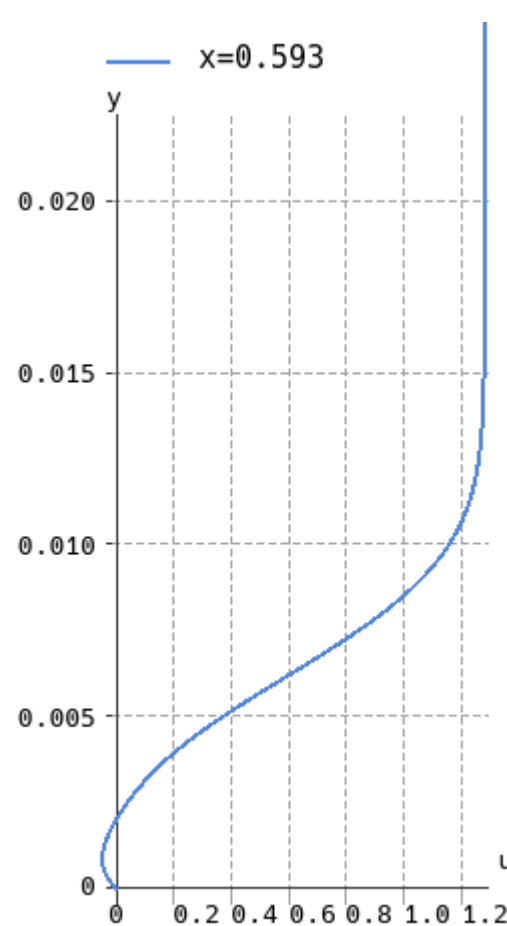
Differential solver



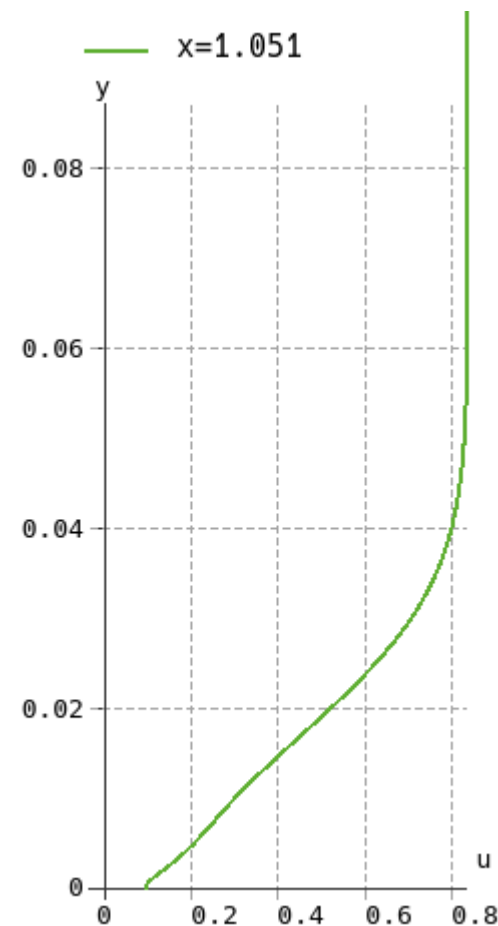
Laminar attached flow
BL thickness ≈ 0.004



Laminar separation
BL thickness ≈ 0.015



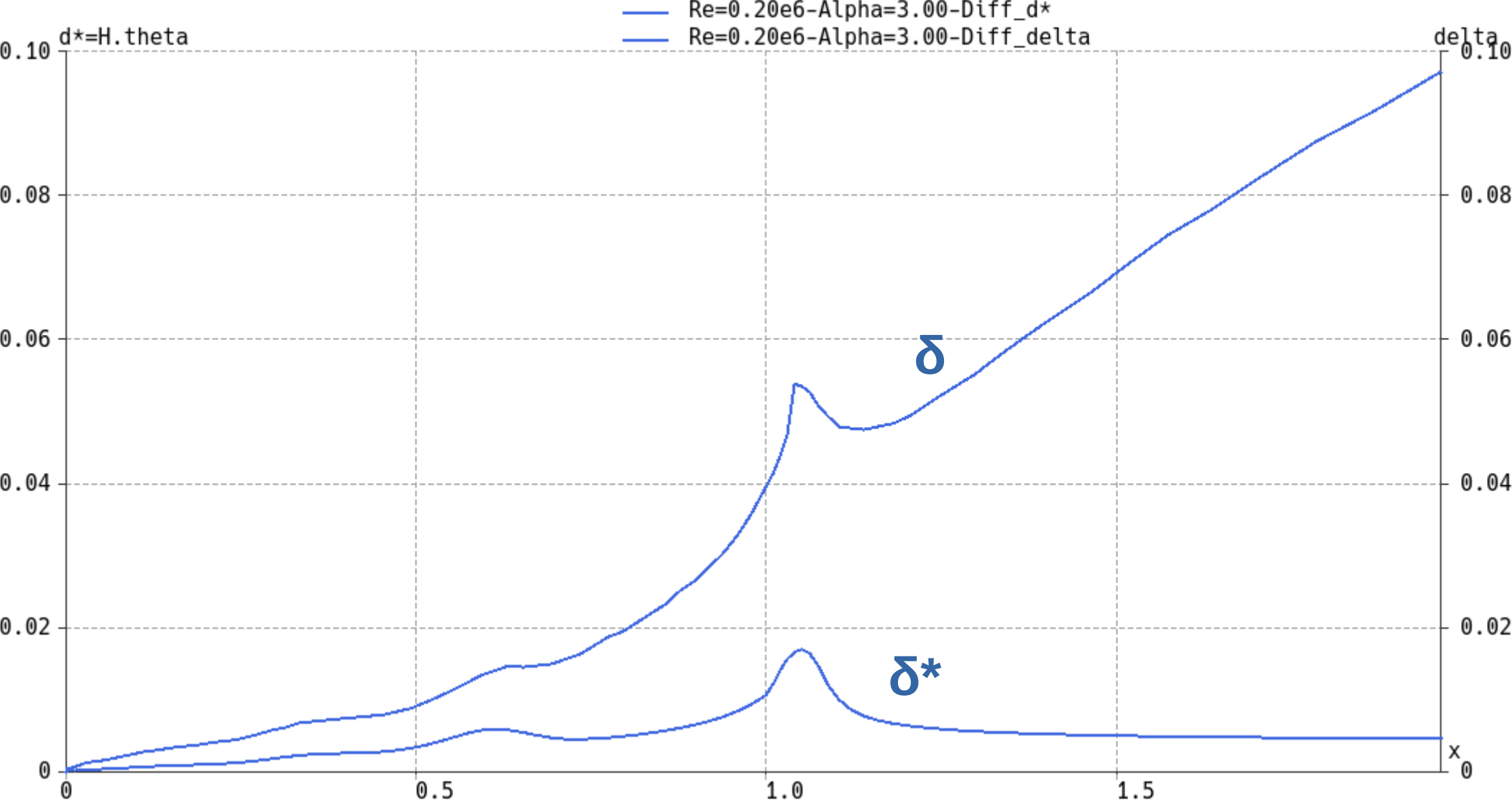
Turbulent separated
BL thickness ≈ 0.020



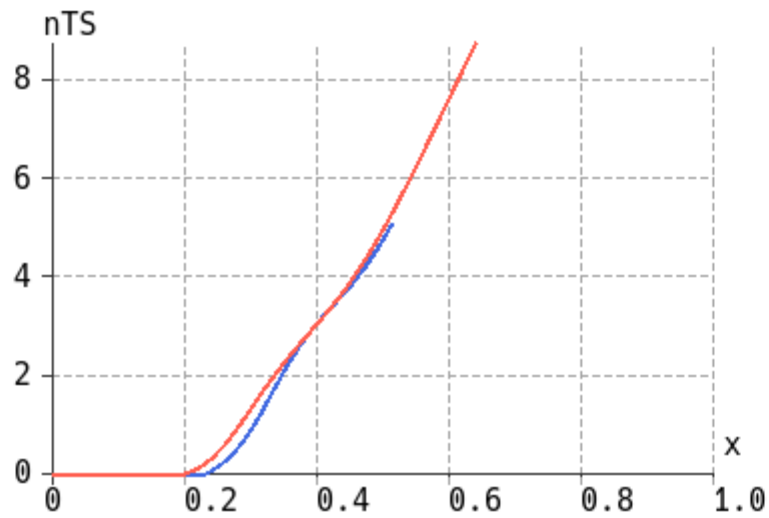
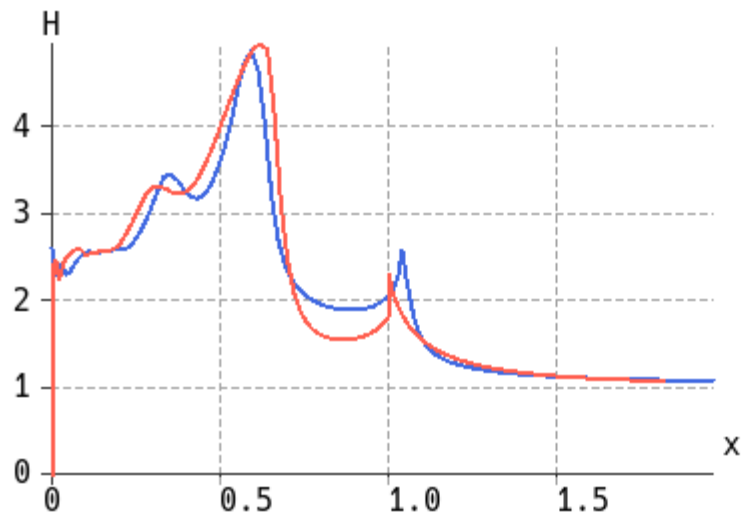
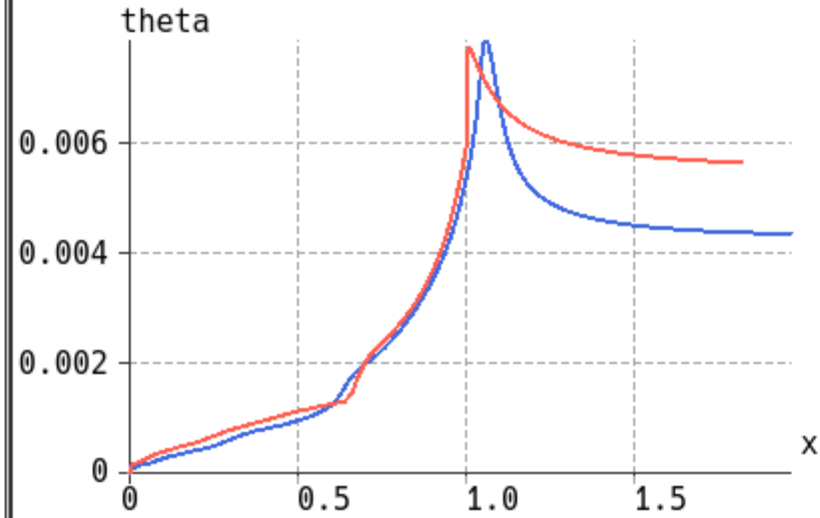
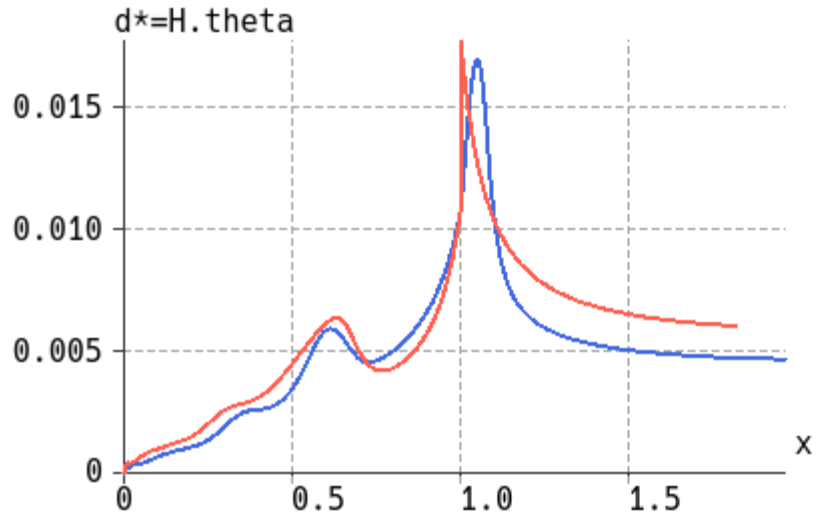
Wake flow
BL thickness ≈ 0.06

Clark Y airfoil, Top surface, $Re=200k$, $aoa=3^\circ$, unit chord length

BL thickness vs. Displacement thickness



XFoil vs. a differential solver



CLARK Y

- Re=0.20e6-Alpha=3.00-Diff
- Re=0.20e6-Alpha=3.00-XFoil

So why does an airfoil drag?

The viscosity creates drag forces by two effects

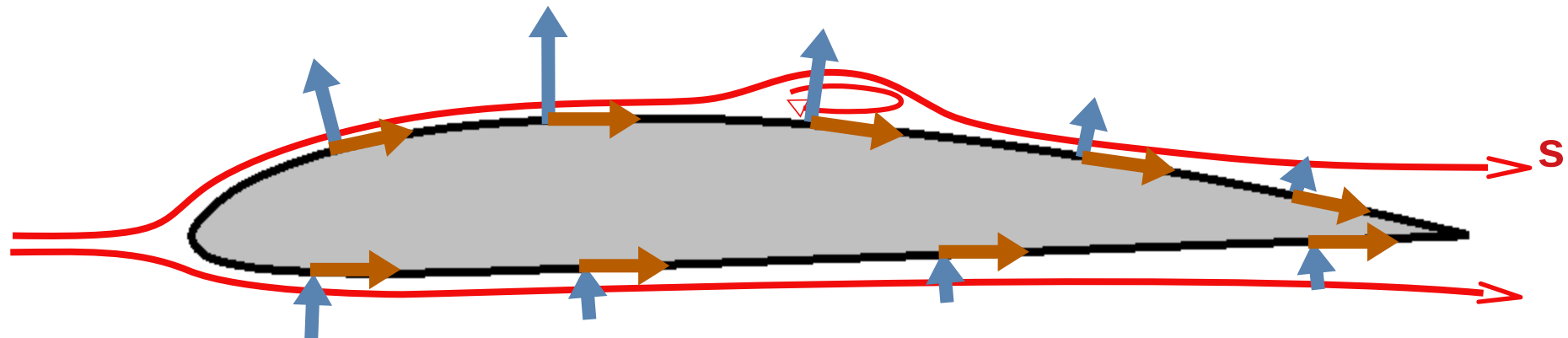
- it creates skin friction forces on the airfoil's surface
- it creates unbalanced pressure forces on the airfoil's surface



“friction drag”



“pressure drag”



Note: The induced drag is a 3d effect only, and is not related to viscosity



pressure forces



skin friction forces

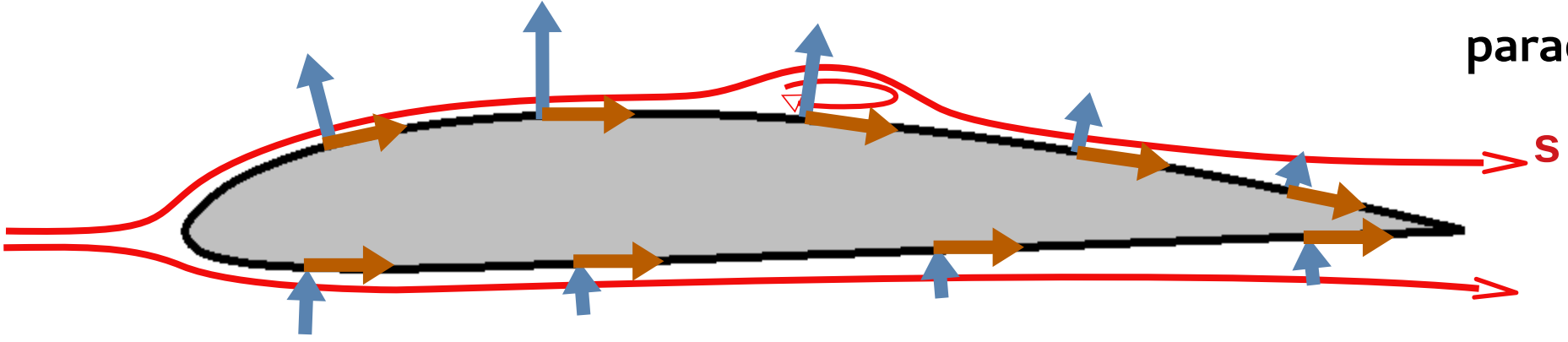
So why does an airfoil drag?

The viscosity creates drag forces by two effects

- it creates skin friction forces on the airfoil's surface
- it creates unbalanced pressure forces on the airfoil's surface

“friction drag” → =0 in inviscid flow: “no viscosity, no friction”

“pressure drag” → =0 in inviscid flow due to d'Alembert's paradox



Note: The induced drag is a 3d effect only, and is not related to viscosity

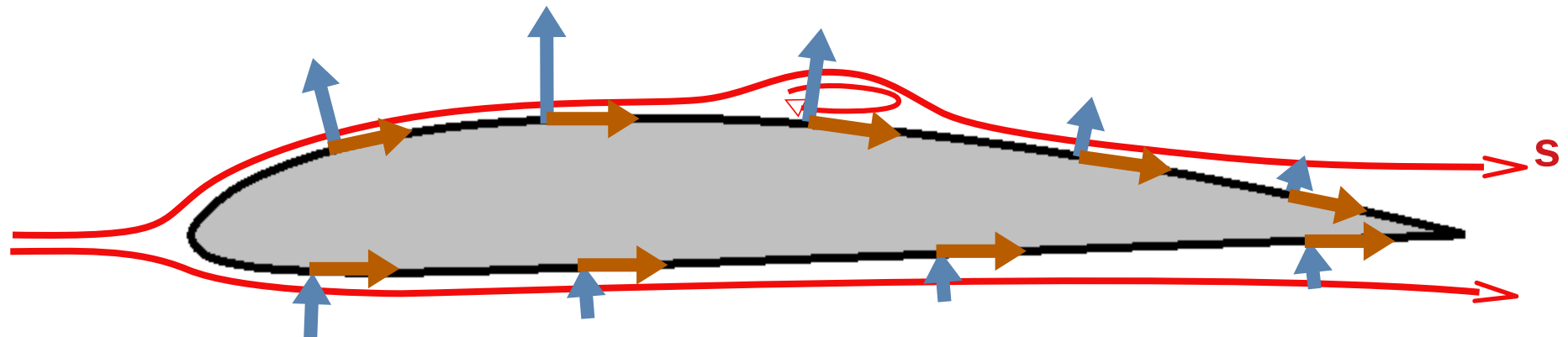
→ pressure forces
→ skin friction forces

So why does an airfoil drag?

“friction drag” + “pressure drag” = “Viscous drag” or “Profile drag”



Both terms are used interchangeably in xflr5



→ pressure forces

→ skin friction forces

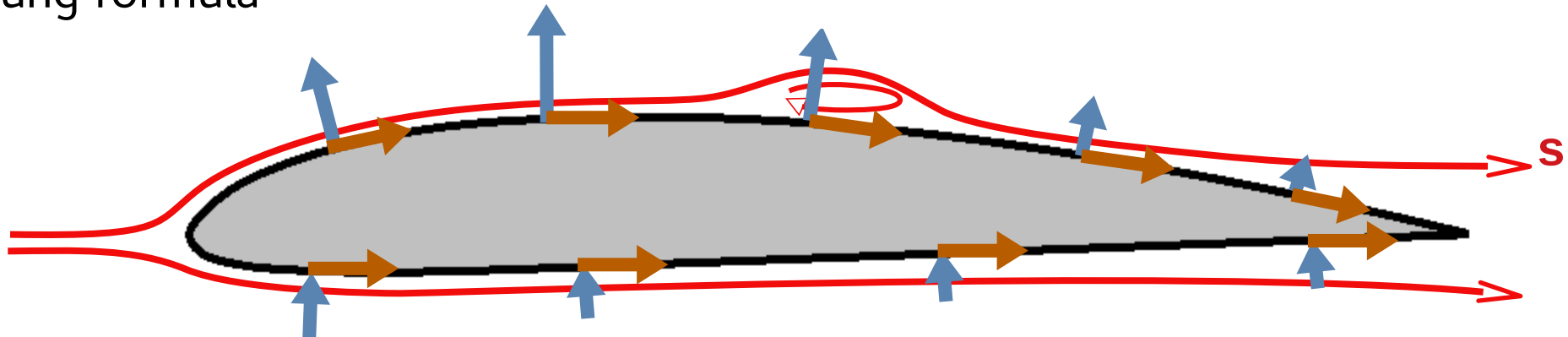
So why does an airfoil drag?

“friction drag” + “pressure drag” = “Viscous drag” or “Profile drag”

Note: The direct evaluation of friction and pressure forces is numerically unreliable; XFOil’s method is to evaluate the total viscous drag in the wake using the Squire-Young formula

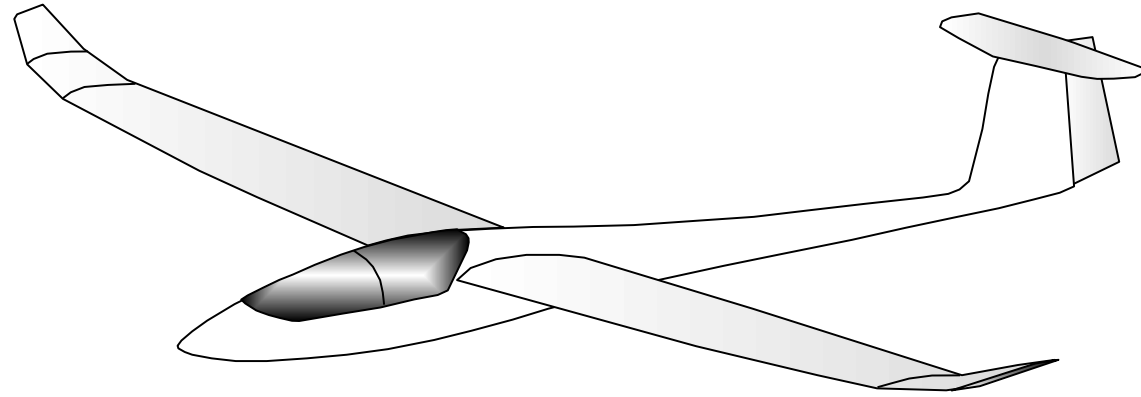
$$C_D = D/q = 2\theta_\infty = 2\theta \left(\frac{u}{V_\infty}\right)^{(H+5)/2}$$

where θ and u
are evaluated at the end of the wake



→ pressure forces

→ skin friction forces



- up next -

Theoretical limitations and shortcomings of xflr5